

Amphitheater Public Schools CDO High School – East Parking Lot Improvements BG Project No: 17.14.66

ADDENDUM 1 – Date: January 13, 2021

This revision shall amend the construction documents and shall become part of the contract. All requirements contained in the original construction documents shall apply to this revision, and the general character of the work called for in this revision shall be the same as originally set forth in applicable portions of the original documents for similar work, unless otherwise specified herein. All work shall be performed as specified in the original documents, even if not particularly mentioned in this revision.

DOCUMENTS ISSUED:

Attachment #1 - Geotechnical Report - Pavement Evaluation

SPECIFICATIONS:

1. Add Geotechnical Report – Pavement Evaluation to Construction Specifications

DRAWINGS:

1. N/A

GENERAL COMMENTS / CLARIFICATIONS:

1. N/A



END OF ADDENDUM #1

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ADDENDUM #1

ATTACHMENT #1



June 3, 2021

Mr. Shane Chism **Breckenridge Group, Inc.** 1735 East Fort Lowell Road, Suite 12 Tucson, Arizona 85719

RE: Geotechnical Report – Pavement Evaluation Canyon de Oro High School East Parking Lot 25 West Calle Concordia Oro Valley, Arizona S&A project Number 211349ST

Dear Mr. Chism:

This letter presents recommendations prepared by Speedie & Associates, Inc. (S&A) for a pavement evaluation for the east parking lot for the Canyon de Oro High School located at 25 West Calle Concordia, Oro Valley, Arizona.

We understand that the east parking lot and the south drop-off lane will be removed and replaced. Based on a review of aerial photos, these areas are approximately 130,000 square feet and approximately 7,000 square feet, respectively. The east parking lot is located at the southeast corner of the Canyon del Oro High School, on the north side of West Calle Concordia. The parking lot has solar powered shade canopies over a majority of parking spots. The ground surface of the lot appears to trend towards the middle of the parking lot from north to south, and is relatively level east to west. The lot is approximately 2 to 3 feet higher in elevation than the south drop-off lane, which trends downwards from east to west, following the grade of West Calle Concordia.

In general, the pavement appears to be in a below average to poor condition. The pavement is exhibiting significant distress including severe stripping (loss of surface fines). This is typically due to an issue with the mix design used and/or poor compaction when installed. Drying shrinkage block cracking is also occurring typical of aged asphalt pavements throughout the entire parking lot and drop off lane. See Photo Log in the Appendix. Block cracking is normal in asphalt pavements. As the asphalt binder (oil) ages, the mix becomes stiffer (less flexible) to the point where the pavement cannot tolerate the daily shrinkage forces that result from temperature changes. Block cracks typically do not represent structural failure. The block-cracked pavement has deteriorated to "alligator" cracking in several areas indicating overstressing and possible subgrade failure. This is typical of progressive failure in part due to lack of maintenance and/or poor drainage that allows water to enter the subgrade resulting in loss of support. Based on field observations, it appears that there has not been a significant effort to maintain the pavement through crack filling or surface treatments.

<u>Geotechnical Evaluation</u>: S&A obtained information about the subsurface conditions at the site using ten (10) hand sample auger soil borings to record the soil conditions and collect samples for laboratory testing. The boring locations were placed in the existing pavement, and were cored with a portable core drill equipped with a 4-inch diameter diamond core barrel to expose the subgrade soils. Bulk soil samples were collected from below the granular fill to depths of up to 3.5 feet below the existing ground surface (bgs). The soil samples were laboratory tested to determine grain-size distribution and plasticity (Atterberg Limits)



for classification and pavement design parameters. The approximate boring locations are shown on the attached Soil Boring Location Plan. The laboratory data is presented in the attached Tabulation of Test Data.

Based on the results of the field and laboratory evaluation, the existing pavement section consists of 3.1 to 4.6 inches of asphaltic concrete in the parking lot area and 1.7 to 2.3 inches of asphaltic concrete in the south drop off lane. The parking lot appears to have been paved in two lifts, with the bottom lift ranging from 1.3 to 2.2 inches and the top lift ranging from 1.5 to 2.7 inches. The south drop off lane appears to have been placed in a single lift. Two to three inches of course-grained gravel with minimal fines were evident below the AC at all locations. This gravel resembles Number 57 rock, typically used underneath Portland Cement Concrete Pavement for drainage purposes. The gravel is underlain by 3 to 5 inches of poorly graded gravel with sand and silt at most locations. Native alluvial soils are evident beneath the pavement sections to the depth of the exploration (4 feet bgs). The alluvium typically consists of silty sand, and occasionally well-graded sand with silt. The samples contain between approximately 6 and 34 percent of material passing the U.S. Standard #200 sieve and were non-plastic. These results correlate to an R-value of 74.

Recommended Minimum Pavement Sections: The subgrade will provide excellent support of the proposed new pavement section, provided that the subgrade is properly compacted and stable, **and adequate surface drainage is provided and maintained**. The pavement section capacity is reported as daily ESALs, (Equivalent 18 kip Single Axle Loads). Heavy vehicles such as school buses, refuse trucks, fire trucks, delivery vans, Class A motor coaches, etc., apply approximately 1 ESAL per vehicle. By comparison, it requires about 1200 autos to apply one ESAL.

The following alternate design parameters and sections are recommended for asphaltic concrete (AC) on aggregate base course (ABC), or Portland cement concrete pavement (PCCP):

	Fle	xible (AC Paver	ment)	Rigid (PCC Pavement)			
Area of Placement	Thie	ckness	Daily 18-kip	Thickness	Daily 18-kip		
	AC (0.39)	ABC (0.12)	ESALs	РССР	ESALs		
	2.0"	4.0	6	5.0"	9		
Auto Parking	3.0" ⁽⁴⁾	None	4	5.5"	15		
	3.0"	4.0"	25	6.0"	23		
Bus/Truck Drives	4.0" ⁽⁴⁾	None	28	6.5"	34		
	4.5"	None	57	7.0"	51		

Notes:

1. Designs are based on AASHTO design equations and ADOT correlated R-Values.

- 2. The PCCP thickness is increased to provide better load transfer and reduce potential for joint & edge failures. Design PCCP per ACI 330R-87.
- 3. Full depth asphalt or increased asphalt thickness can be increased by adding 1.0-inch asphalt for each 3 inches of base course replaced.
- 4. These represent the approximate existing pavement sections.



Pavement Design Parameters

Assume:	One 18 kip Equivalent Single Axle Load (ESAL)/Truck
Life:	20 years
Subgrade Soil Profile:	
Material Passing #200 sie	eve: 23 Percent (Ave.)
Plasticity Index:	Non-plastic (Ave.)
k:	150 pci (assumed)
R value:	74 (per ADOT tables)
M_R :	26,000 (Maximum Allowed per AASHTO Design)

The designs presented the table above assume that all subgrade areas are properly prepared in accordance with the recommendations outlined in this report.

The entire area to be occupied by the proposed construction should be stripped of all vegetation, debris, asphalt, rubble, obviously loose surface soils, (fill, foundations, etc. if any are encountered), and any other deleterious materials. The existing asphaltic concrete may be cold-milled in-place to a gradation like that of an ABC and stockpiled for reuse under new paved areas as sub-base.

The soils are moisture sensitive and the exposed subgrade may become unstable depending on the moisture content at the time of construction. If areas of elevated moisture exists, there is a potential for the soils to become soft and unstable. Several options are available to remedy this condition including deep ripping to open the wet subgrade and allow the soils time to dry, or removal and replacement of the wet, soft soils with suitable materials. If instability extends too deep, replacement can be combined with at least 12 inches of granular fill (ABC and/or millings) with geogrid such as Tensar Triax installed per the manufacturer's recommendations. Or cement could be used to create a cement-treated subgrade. Prior to placement of the aggregate base course, the pavement subgrade could be proof rolled with a 5,000 gallon water truck (or similar vehicle) to determine if there are soft areas.

After grading to provide proper drainage the exposed grades should be scarified a minimum of 8 inches deep. The scarified soils should be thoroughly and uniformly moisture conditioned to ± 2 percent of the material's optimum moisture content and compacted to at least 95 percent of its maximum dry density as determined by ASTM D-698 laboratory test procedures. If fill is required, the fill should be placed in horizontal lifts of a maximum of 8-inch loose thickness (or less depending on the compaction equipment) properly moisture conditioned as described above and compacted to at least 95 percent of the material's maximum dry density per ASTM D-698. Aggregate base course should be properly moisture conditioned and compacted to a minimum of 100 percent of the material's maximum dry density per ASTM D-698.

Silty fine sand soils may be exposed and may be sensitive to excessive moisture content and will become unstable at elevated moisture content. Accordingly, it may be necessary to compact soils on the dry side of optimum. The reduced moisture content under slabs-on-grade should only be used upon approval of the engineer in the field.



Asphaltic concrete pavement base course material should be per Pima County/City of Tucson (PAG/COT) Section 303 Specifications. Asphaltic concrete materials and mix design should conform to PAG/COT Section 406. It is recommended that mix designation No. 2 or No. 3 be used for the pavements. While the No. 2 mix has a somewhat rougher texture, it tends to offer more stability and resistance against surface scuffing, particularly in truck turning areas. Pavement installation should be carried out under applicable portions of PAG/COT Section 406 and municipality standards. The asphalt supplier should be informed of the pavement use and required to provide a mix that will provide stability and be aesthetically acceptable. Some of the newer mixes are very coarse and could cause placing and finish problems. A mix design should be submitted for review to determine if it will be acceptable for the intended use.

Portland Cement Concrete Pavement must have a minimum 28-day flexural strength 550 psi (compressive strength of approximately 3,700 psi). It may be cast directly on the prepared subgrade with proper compaction. Lacking an aggregate base course, attention must be paid to using low slump concrete and proper curing, especially on the thinner sections. No reinforcing is necessary. Joint design and spacing should be in accordance with ACI recommendations. Construction joints should contain dowels or be tongue and grooved to provide load transfer. Tie bars are recommended on the joints adjacent to unsupported edges. Maximum joint spacing in feet should not exceed 2 to 3 times the thickness in inches. Joint sealing with a quality silicone sealer is required recommended to prevent water from entering the subgrade allowing pumping and loss of support. If not sealed, add a nominal 4-inch ABC subbase.

Proper subgrade preparation and joint sealing will reduce (but not eliminate) the potential for slab movements (thus cracking) on the native soils. Frequent jointing will reduce uncontrolled cracking and increase the efficiency of aggregate interlock joint transfer.

It must be noted that all new asphalt pavements will eventually crack. Cracking in asphalt pavement is typical and should be expected over the life of the pavement. In fact, it has been our experience of late that the new asphalt binders that are available, we are seeing the onset or earlier aging and cracking. These require routine maintenance to prevent accelerated deterioration. Accordingly, it is highly recommended to establish a maintenance program where the cracks are routinely filled, as they appear beginning at about the second year of life. It is also recommended that surface fog seal coats be considered beginning at about year 5 and every 5 years after. This will help preserve the pavements, extending the service life.



General: Our analysis of data and the recommendations presented herein are based on the assumption that soil conditions do not vary significantly from those found at specific sample locations. Our work has been performed in accordance with generally accepted engineering principles and practice; this warranty is in lieu of all other warranties express or implied.

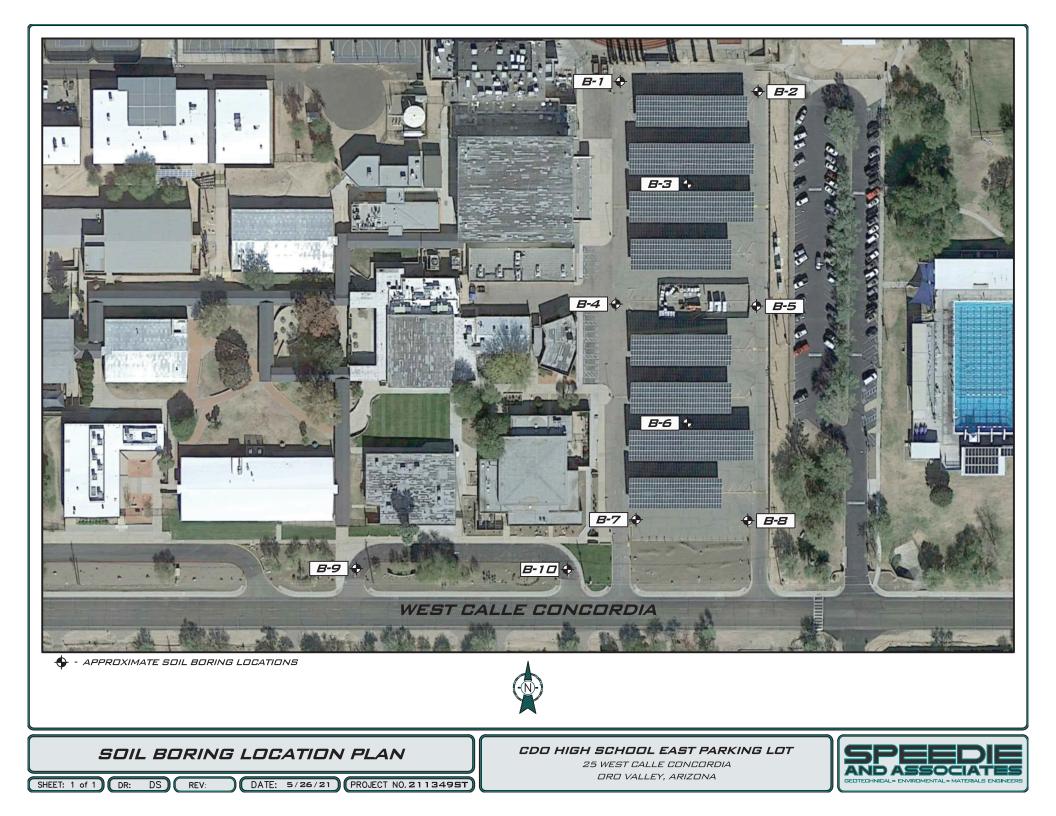
We recommend that a representative of the Geotechnical Engineer observe and test the earthwork and pavement portions of this project to ensure compliance to project specifications and the field applicability of subsurface conditions which are the basis of the recommendations presented in this report. If any significant changes are made in the scope of work or type of construction that was assumed in this report, we must review such revised conditions to confirm our findings if the conclusions and recommendations presented herein are to apply.

We trust this meets your needs. If there are any questions, please call.

Respectfully Submitted, **SPEEDIE & ASSOCIATES, INC.**

Daniel Stratulat, E.I.T. Staff Engineer Gregg A Creaser, P.E. Principal

Attachments: Boring Location Plan, Boring Logs, Laboratory Data, Photo Log

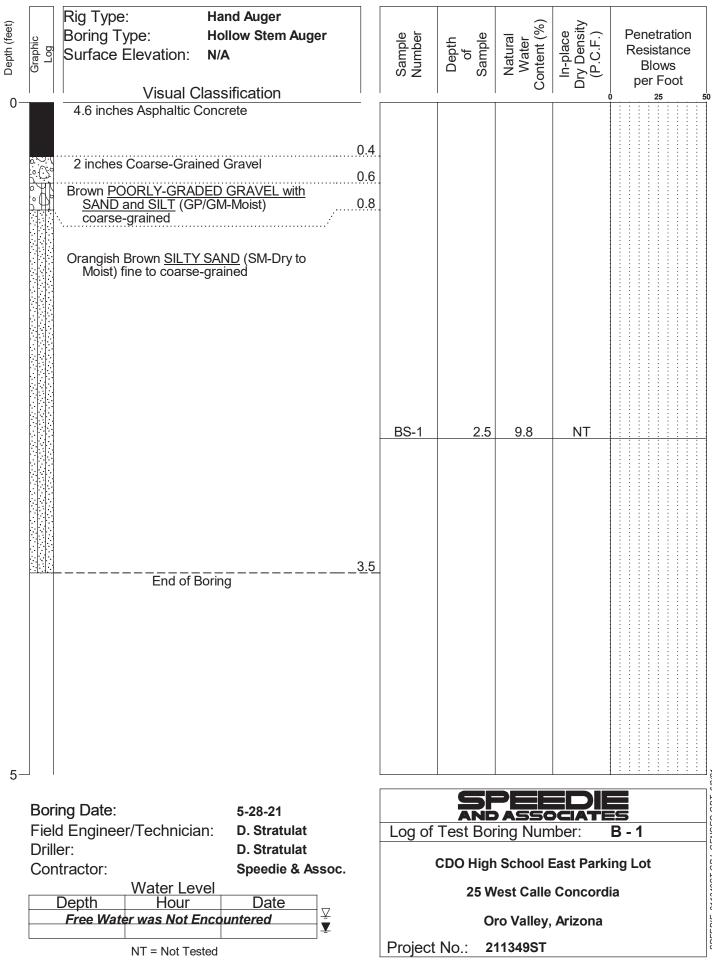


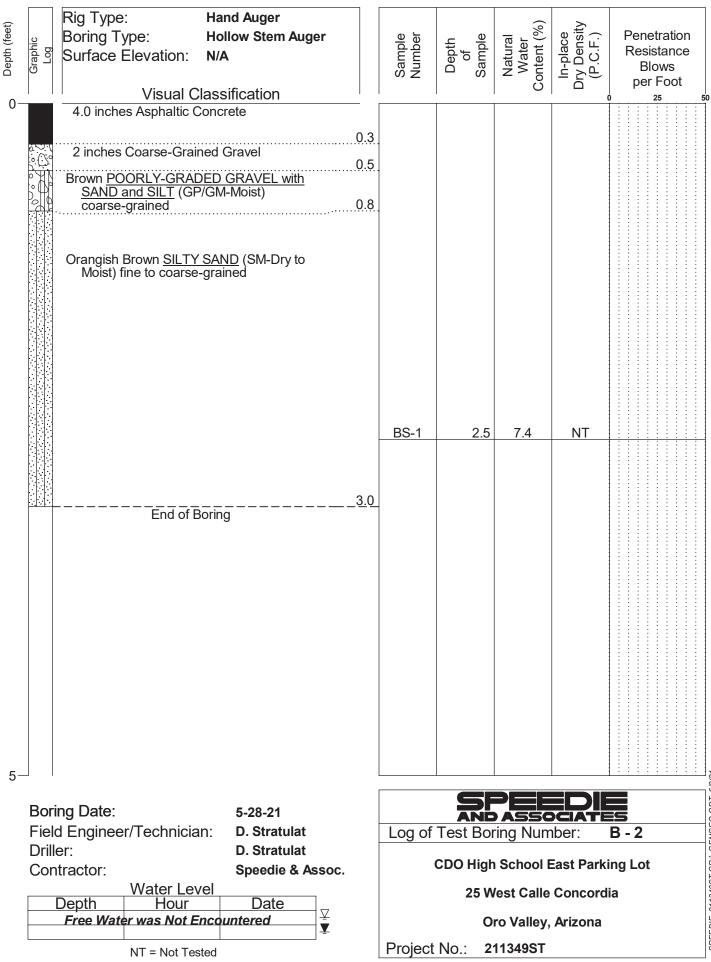
SOIL LEGEND

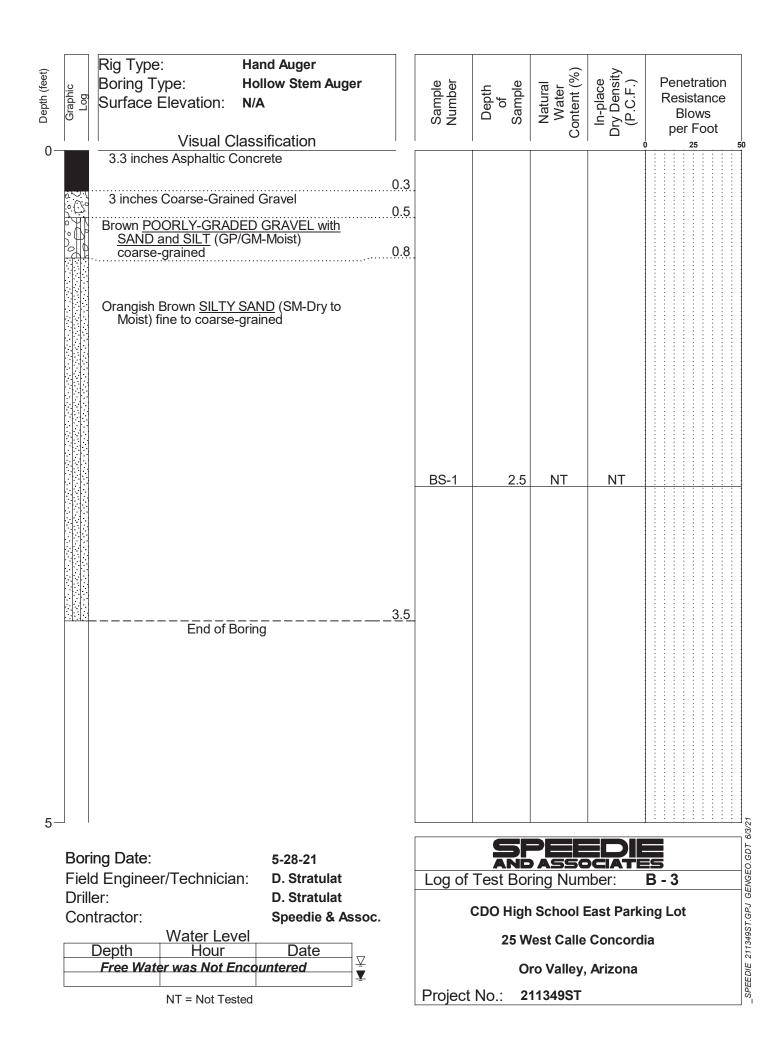
D	SAMPLE ESIGNATION		DESCRIPTION
$\left\{ \right\}$	AS	Auger Sample	A grab sample taken directly from auger flights.
\mathbf{R}	BS	Large Bulk Sample	A grab sample taken from auger spoils or from bucket of backhoe.
	S	Spoon Sample	Standard Penetration Test (ASTM D-1586) Driving a 2.0 inch outside diameter split spoon sampler into undisturbed soil for three successive 6-inch increments by means of a 140 lb. weight free falling through a distance of 30 inches. The cumulative number of blows for the final 12 inches of penetration is the Standard Penetration Resistance.
	RS	Ring Sample	Driving a 3.0 inch outside diameter spoon equipped with a series of 2.42-inch inside diameter, 1-inch long brass rings, into undisturbed soil for one 12-inch increment by the same means of the Spoon Sample. The blows required for the 12 inches of penetration are recorded.
	LS	Liner Sample	Standard Penetration Test driving a 2.0-inch outside diameter split spoon equipped with two 3-inch long, 3/8-inch inside diameter brass liners, separated by a 1-inch long spacer, into undisturbed soil by the same means of the Spoon Sample.
X	ST	Shelby Tube	A 3.0-inch outside diameter thin-walled tube continuously pushed into the undisturbed soil by a rapid motion, without impact or twisting (ASTM D-1587).
		Continuous Penetration Resistance	Driving a 2.0-inch outside diameter "Bullnose Penetrometer" continuously into undisturbed soil by the same means of the spoon sample. The blows for each successive 12-inch increment are recorded.

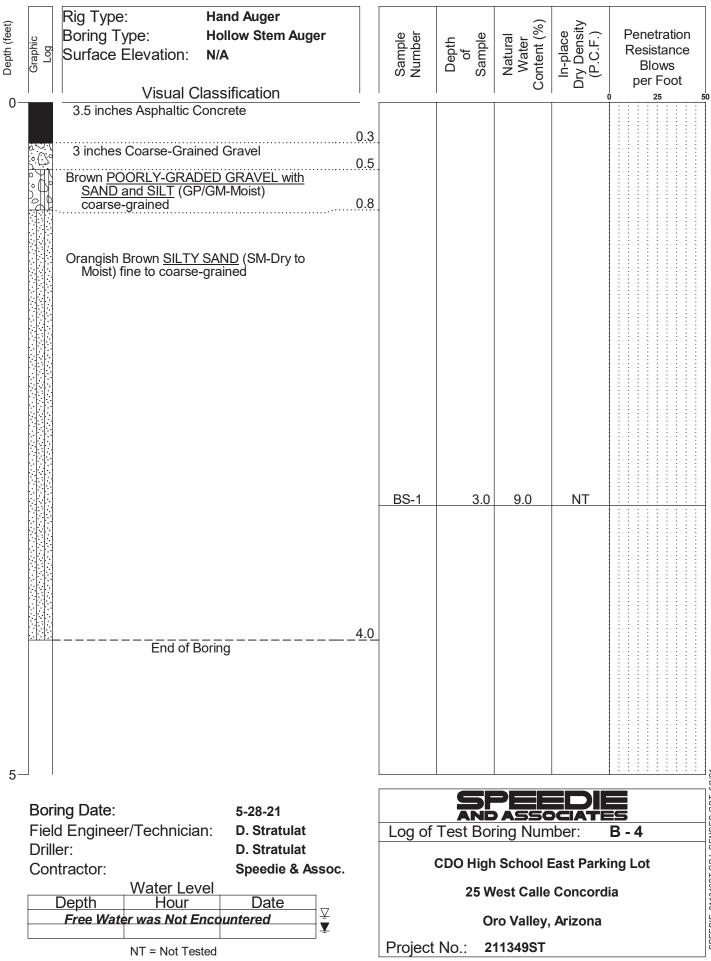
	CONSISTENCY	RELATIVE DENSITY				
Clays & Silts	Blows/Foot	Strength (tons/sq ft)	Sands & Gravels	Blows/Foot		
Very Soft Soft Firm Stiff Very Stiff Hard	0 - 2 2 - 4 5 - 8 9 - 15 16 - 30 > 30	0 - 0.25 0.25 - 0.5 0.5 - 1.0 1 - 2 2 - 4 > 4	Very Loose Loose Medium Dense Dense Very Dense	0 - 4 5 - 10 11 - 30 31 - 50 > 50		

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IVI		5115	GRAPH	LETTER	DESCRIPTIONS		MATE	RIAL	<u> </u>					:4
	GRAVEL	CLEAN GRAVELS		GW	WELL-GRADED GRAVELS, GRAVEL - SAND MIXTURES, LITTLE OR NO FINES		SIZ		Lo	Lower Limit m Sieve Size +		Upper Limi mm Sieve Siz		
	AND GRAVELLY SOILS	(LITTLE OR NO FINES)		GP	POORLY-GRADED GRAVELS, GRAVEL - SAND MIXTURES, LITTLE OR NO FINES		SANDS Fine		0.075	#200		0.42	#40	20
COARSE GRAINED SOILS	MORE THAN 50% OF COARSE FRACTION	GRAVELS WITH FINES		GM	SILTY GRAVELS, GRAVEL - SAND - SILT MIXTURES		Med Coa	ium	0.075	#200 #40 #10		0.42 2.00 4.75	#40 #10 #4	
00120	RETAINED ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		GC	CLAYEY GRAVELS, GRAVEL - SAND - CLAY MIXTURES		GRA							
MORE THAN 50% OF	SAND	CLEAN SANDS		, sw	WELL-GRADED SANDS, GRAVELLY SANDS, LITTLE OR NO FINES		Fir	ne	4.75 19	#4 0.75"	×	19 75	0.75' 3"	' × ×
MATERIAL IS LARGER THAN NO. 200 SIEVE SIZE	AND SANDY SOILS	(LITTLE OR NO FINES)		SP	POORLY-GRADED SANDS, GRAVELLY SAND, LITTLE OR NO FINES		COBBLES			3"	×	300	12"	×
C	MORE THAN 50% OF COARSE FRACTION	SANDS WITH FINES		SM	SILTY SANDS, SAND - SILT MIXTURES		BOUL	DERS	300	12"	×	900	36"	×
	PASSING ON NO. 4 SIEVE	(APPRECIABLE AMOUNT OF FINES)		sc	CLAYEY SANDS, SAND - CLAY MIXTURES	♦U.S. Standard		Standard		×CI	ear S	Square	Opening	js
				ML	INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS OR CLAYEY SILTS WITH SLIGHT PLASTICITY		60							7
FINE	SILTS AND CLAYS	LIQUID LIMIT LESS THAN 50		CL	INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAYS	-	50							
GRAINED SOILS	CLATS			OL	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY	Plasticity	40			B-Line	СН			
MORE THAN 50% OF MATERIAL IS				мн	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE SAND OR SILTY SOILS		30			- P	me			
SMALLER THAN NO. 200 SIEVE SIZE	SILTS AND CLAYS	LIQUID LIMIT GREATER THAN 50		сн	INORGANIC CLAYS OF HIGH PLASTICITY	Index	20	C	L	\square		MH & O	н	
	OLATO			ОН	ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS	×	10	CL-ML						
н	GHLY ORGANIC S	OILS		РТ	PEAT, HUMUS, SWAMP SOILS WITH HIGH ORGANIC CONTENTS		0	20	4	^{& OL}	0	80	10	00
OTE: DUAL (OR MODIFIED S	YMBOLS MAY B	 E USED 1	O INDICAT	E BORDERLINE SOIL					Liquid L	imit			



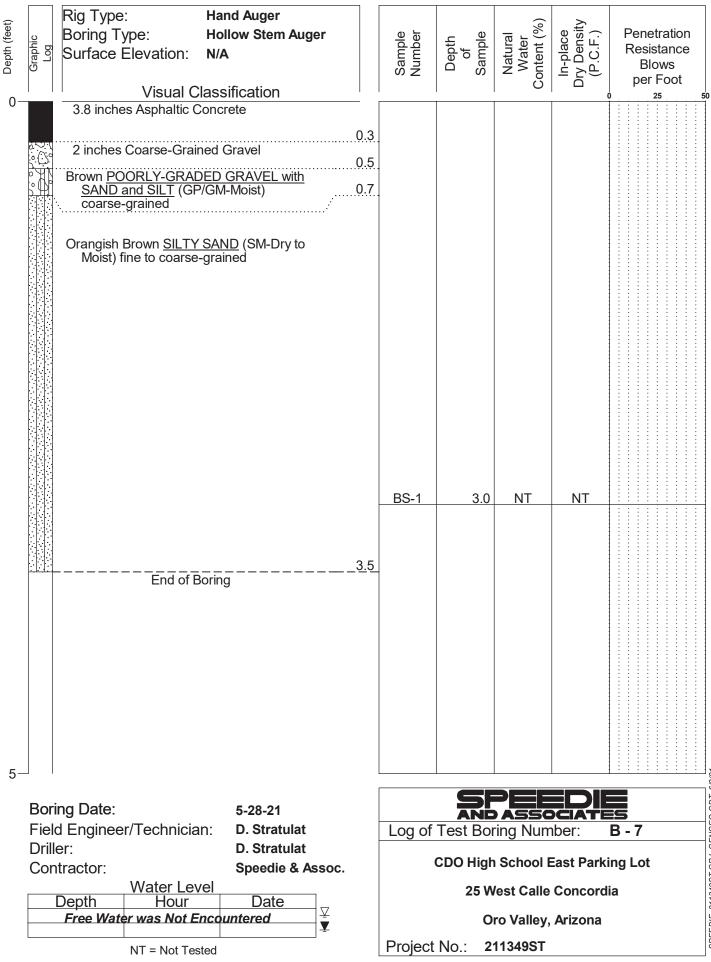






Depth (feet)	Graphic Log	Rig Type: Hand Auger Boring Type: Hollow Stem Auger Surface Elevation: N/A	Sample Number	Depth of Sample	Natural Water Content (%)	In-place Dry Density (P.C.F.)	Penetration Resistance Blows per Foot
0-		Visual Classification 3.7 inches Asphaltic Concrete				Ċ	25 50
		0.3 3 inches Coarse-Grained Gravel 0.6					
		Orangish Brown <u>SILTY SAND</u> (SM-Dry to Moist) fine to coarse-grained					
		With gravel below 2.5 feet) BS-1	3.0	NT	NT	
		End of Boring				-	
5-							721
	. .			SF	ÞEE		
		ng Date: 5-28-21 d Engineer/Technician: D. Stratulat					
	Drille			Test Bor CDO High			B - 5 ng Lot
		Water Level		25 W	est Calle	Concord	ia
		Depth Hour Date Free Water was Not Encountered ☑		0	ro Valley,	Arizona)IE 211
		NT = Not Tested	Project		11349ST		SPEEL

Depth (feet) Graphic Log	Rig Type:Hand AugerBoring Type:Hollow Stem AugerSurface Elevation:N/AVisual Classification	Sample Number	Depth of Sample	Natural Water Content (%)	In-place Dry Density (P.C.F.)	Penetration Resistance Blows per Foot		
	3.1 inches Asphaltic Concrete 0.3 2 inches Coarse-Grained Gravel 0.4 Brown POORLY-GRADED GRAVEL with SAND and SILT (GP/GM-Moist) coarse-grained 0.8 Orangish Brown SILTY SAND (SM-Dry to Moist) fine to coarse-grained 0.8							
	3.5 End of Boring	5 BS-1	3.5	4.1	NT			
5Borii	ng Date: 5-28-21		SF			B - 6 ng Lot ia		
	Bengineer/Technician: D. Stratulat	Log of	Test Bo			B - 6		
	tractor: Speedie & Assoc. Water Level		CDO High			ng Lot		
	Depth Hour Date	25 West Calle Concordia Oro Valley, Arizona						
	NT = Not Tested	Project		ro valley, 11349ST				



Depth (feet) Graphic Log	Rig Type:Hand AugerBoring Type:Hollow Stem AugerSurface Elevation:N/AVisual Classification	Sample Number	Depth of Sample	Natural Water Content (%)	In-place Dry Density (P.C.F.)	Penetration Resistance Blows per Foot
0-	4.5 inches Asphaltic Concrete					0 25 50
	0.4 2 inches Coarse-Grained Gravel 0.5 Brown <u>POORLY-GRADED GRAVEL with</u> <u>SAND and SILT</u> (GP/GM-Moist) coarse-grained 0.8 Auger Refusal on Gravel	BS-1	1.0	NT	NT	
5						
			SF	PEE		
	ing Date: 5-28-21 d Engineer/Technician: D. Stratulat	l og of	Test Bor	ASSC		S B - 8
Dril						
	ntractor: Speedie & Assoc.		CDO High	School E	East Parki	ing Lot
	Water Level Depth Hour Date Free Water was Not Encountered ✓			/est Calle ro Valley,	Concord	ia
	NT = Not Tested	Proiect	No.: 2'	-		

NI = Not lested

B ic (feet		Hand Auger Hollow Stem Auger N/A	Sample Number	Depth of Sample	Natural Water Content (%)	In-place Dry Density (P.C.F.)	Penetration Resistance Blows per Foot 25 50
a	1.7 inches Asphaltic C 2 inches Coarse-Grain Brown <u>POORLY-GRAE</u> <u>SAND and SILT</u> (GF coarse-grained	ned Gravel 0	3				
ده می و وروند می و وروند می و وروند می و وروند. موروند می و وروند می و وروند می و وروند می و و و و و و و و و و و و و و و و و و و	Drangish Brown <u>WELL</u> <u>SILT</u> (SW/SM-Dry to coarse-grained	-GRADED SAND with Moist) fine to					
			<u>5 BS-1</u>	2.5	3.8	NT	
5	Drangish Brown <u>SILTY</u> Moist) fine to coarse End of E	4	0				
-	g Date:	5-28-21			ASSC		
Driller		D. Stratulat	Log of	Test Boi			B - 9 ing Lot ia
Contra	Water Lev	Speedie & Assoc. /el		CDO High 25 W		Concord	ia
	epth Hour Free Water was Not E	Date □ Countered □ ✓			ro Valley,		
	NT = Not Tes		Projec	t No.: 2	11349ST		

Depth (feet)	Graphic Log	Rig Type: Boring Type: Surface Elevation: Visual C	Hand Auger Hollow Stem Auger N/A lassification	Sample Number	Depth of Sample	Natural Water Content (%)	In-place Dry Density (P.C.F.)	Penetration Resistance Blows per Foot
0-		2.3 inches Asphaltic C 2 inches Coarse-Grain Brown <u>POORLY-GRAE</u> <u>SAND and SILT</u> (GF coarse-grained Orangish Brown <u>SILTY</u> Moist) fine to coarse	Concrete 0.2 ned Gravel 0.4 <u>DED GRAVEL with</u> 7/GM-Moist) 0.7) 25 50
5-		End of B	<u>3.0</u> Roring	BS-1	2.5	4.8	NT	
		ng Date:	5-28-21 n: D. Stratulat					S 40
	Drill	d Engineer/Technicia er: tractor:	D. Stratulat D. Stratulat Speedie & Assoc.		Test Boi CDO High			B -10 ing Lot
		Water Lev Depth Hour	-		_		Concord	-
		Free Water was Not E			0	ro Valley,	Arizona	
		NT = Not Tes	ited	Project	No.: 2	11349ST		

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				ENT		PAR		SIZE DIS cent Fi	STRIBU iner)	TION		IERBE			
SOIL BORING or TEST PIT NUMBER	SAMPLE NUMBER	SAMPLE TYPE	SAMPLE INTERVAL (ft)	NATURAL WATER CONTENT (Percent of Dry Weight)	IN-PLACE DRY DENSITY (Pounds Per Cubic Foot)	#200 SIEVE	#40 SIEVE	#10 SIEVE	#4 SIEVE	3" SIEVE	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	UNIFIED SOIL CLASSIFICATION	SPECIMEN DESCRIPTION
B - 1	BS-1	BULK	1.0 - 2.5	9.8	NT	32.8	60	87	95	100	NP	NP	NP	SM	SILTY SAND
B - 2	BS-1	BULK	1.0 - 2.5	7.4	NT	33.3	60	85	93	100	NP	NP	NP	SM	SILTY SAND
B - 4	BS-1	BULK	1.0 - 3.0	9.0	NT	31.3	57	84	92	100	NP	NP	NP	SM	SILTY SAND
B - 6	BS-1	BULK	1.0 - 3.5	4.1	NT	16.2	42	76	90	100	NP	NP	NP	SM	SILTY SAND
B - 9	BS-1	BULK	1.0 - 2.5	3.8	NT	6.5	23	73	92	100	NP	NP	NP	SW-SM	WELL-GRADED SAND with SILT
B -10	BS-1	BULK	1.0 - 2.5	4.8	NT	16.0	40	79	93	100	NP	NP	NP	SM	SILTY SAND
NT=Not	eve analysis results do not include material greater than 3". Refer to the tual boring logs for the possibility of cobble and boulder sized materials. T=Not Tested neet 1 of 1											ool Easi Concore ona 349ST		ig Lot	SPEEDIE AND ASSOCIATES

APPENDIX A: Surface Photographs



Photo No. 1: Stripping close up.



Photo No. 3: Drop off lane.



Photo No. 5: Drive lane typical.



Photo No. 2: Conditions under canopies



Photo No. 4: Drop off lane close up.



Photo No. 6: Alligator cracking typical.